

#### Matching Heat Pumps to Heating & Cooling Profiles in the NZ Food Processing Sector

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# Process Heating in NZ

- 34% NZ energy consumption
- 27% NZ energy-related GHG emissions (2<sup>nd</sup> behind transport)
- $\sim 60\%$  is supplied by burning fossil fuels; mainly in boiler systems
- Also:
  - domestic hot water =  $\sim 4\%$  NZ energy
  - spacing heating of commercial & public building via hot water =  $\sim 5\%$  NZ energy





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# Food Industry Process Heating

- ~25% of NZ process heating across ~200 sites (Atkins, 2019)
- most at temperatures less than 200°C
  - < 100°C hot water, cleaning, blanching, pasteurization, concentration
  - 100-150°C sterilisation, cooking, drying
  - >150°C cooking, drying
- decarbonising options
  - demand reductions
  - electro-technologies e.g. microwave, ohmic, PEF, UV etc
  - heat recovery by heat exchange (HX)
  - heat pumps (HPs)



# HP Feasibility Criteria

• Economic

 $\text{COP} > \frac{\text{cost of electricity}}{\text{cost of fuel}} \times \eta_{\text{fuel to useful heat}}$ 

• Environmental (e.g. CO<sub>2</sub>)

$$\text{COP} > \frac{EF_{\text{electricity}}}{EF_{\text{fuel for heat}}} \times \eta_{\text{fuel to useful heat}}$$

- $EF = \text{emissions factor } (\text{kt CO}_{2eq}/\text{PJ}; \text{g CO}_{2eq}/\text{MJ})$
- need to include production, transmission, distribution & standing losses
- extra capital vs savings in energy costs and emissions



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# Examples of Use of HP Criteria

- natural gas boiler vs electrical HP in NZ
  - electricity @ \$0.12/kWh
  - gas @ \$11/GJ (\$0.04/kWh)
  - $\eta_{\text{gas to heat}} = 80\%$  (non-condensing boiler)
- economic criteria

$$COP > \frac{\text{cost of electricity} \times \eta_{\text{fuel to useful heat}}}{\text{cost of fuel}} = \frac{0.12}{0.04} \times 0.8 = 2.4$$

• environmental (carbon)

$$COP > \frac{EF_{electricity}}{EF_{fuel \text{ for heat}}} \times \eta_{fuel \text{ to useful heat}} = \frac{30}{54} \times 0.8 = 0.4 \quad (\approx 3.5 \text{ in Oz})$$

and even if marginal electricity is CCGT  $(\eta_{gas to electricity} = 50\%)$ 

$$COP > \frac{54}{54} \times \frac{0.8}{0.5} = 1.6$$

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Fuel	Emission Factor			
Natural Gas	54 g CO <sub>2eq</sub> /MJ			
LPG	$60 \mathrm{g} \mathrm{CO}_{\mathrm{2eq}}/\mathrm{MJ}$			
Coal – bituminous	89 g CO <sub>2eq</sub> /MJ			
Coal – sub-bituminous	92 g CO <sub>2eq</sub> /MJ			
Coal – lignite	93 g CO <sub>2eq</sub> /MJ			
Electricity (2018)	30 g CO <sub>2eq</sub> /MJ			
	108 g/kWh			
Electricity (2016)	98 g/kWh			
Electricity (2014)	127 g/kWh			

**MBIE (2019b)** 

# HP Potential

- Carnot Efficiency (excluding HX, fans and pumps)
- 50% of  $\text{COP}_{\text{Carnot}}$  realistic if include HX, fans & inefficiencies
- Use log-mean absolute temperatures if glides in sink or source temperatures

$$\text{COP}_{\text{carnot}} = \frac{T_{hot} + 273}{T_{hot} - T_{cold}}$$

 $COP_{carnot} = \frac{75 + 273}{75 - 5} = 34.8$ 



#### • Examples:

- ambient source to 95°C water
- $T_{cold} = 20^{\circ} \text{C}, \ T_{hot} = 95^{\circ} \text{C}$
- waste heat source to 60°C water
- $T_{cold} = 30^{\circ}\text{C}, T_{hot} = 60^{\circ}\text{C}$
- evaporator MVR evaporated water at 65°C; steam at 75°C

COP<sub>carnot</sub>

- $T_{cold} = 65^{\circ}\text{C}, \ T_{hot} = 75^{\circ}\text{C}$
- Temperature lifts  $< \approx 60^{\circ}$ C for COP<sub>actual</sub> > 3
- Need good temperature matching to get high COP



 $\text{COP}_{\text{carnot}} = \frac{95 + 273}{95 - 20} = 4.9$  (9.1 if transcritical)

 $=\frac{60+273}{60-30}=11.1$ 

Kobelco SGH 120/165
Kobelco HEM-HR90
HeatBooster S4
Ochsner IWWDSS R2R3b
Ochsner IWWDS ER3c4
Ochsner IWWDS ER3c4
Hybrid Heat Pump
Junitop 22/22
∆ Combitherm
GEA Grasso FX P
Star Refrigeration Neatpump
SABROE HeatPAC HPX
Vitocal 350-HT Pro
△ Mitsubishi ETW-L

Aspagaus et al (2018)

### Case Study Analysis Methodology



- Pinch technology methods used to develop GCCs for typical sites
- Process to process heat recovery given priority over HPs
- HP placed across the pinch
  - below 20°C use refrigeration rejecting @ 25°C to HP or to ambient @ 15°C or a HP
  - HP cycle chosen to match heat sources and sinks (e.g. sub-critical if near constant temp; trans-critical or hybrid absorption-compression if across temp ranges)
  - refrigerants to match temp range (standard equipment pressure, high efficiency)
  - $\circ \max T_e$  and  $\min T_c$  yet fit GCC
  - size HP to maximise limiting heat flow (cooling or heating) i.e. all cooling & heating useful
  - multi-staging or cascades if PR>6 (>1.5 for R718)
  - ambient if HP waste sources limiting
  - o residual heating & cooling using traditional boilers or refrigeration



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### **Options and Assumptions**

- Refrigerants & Cycles
  - $\circ\,$  R717 up to 60 bar
  - $\circ$  R744 up to 150 bar with IHX
  - multi-stage R718 above 70°C
  - hybrid absorption-compression R717-R718
  - o other refrigerants if better matches e.g. R600, R134a, R245fa, R1336mzz(Z), R1234ze(E)

#### • Technical & Economic Data

- o 75% isentropic efficiency for compressor, pumps, turbines
- $\circ\,$  negligible heat losses, pressure drops, SH and SC
- $\circ$  energy for ambient cooling @ 3% of heat of rejection
- $\circ$  HP or refrigeration capital = NZ1000/kW
- $\circ$  electricity @ \$0.12/kWh; EF=30 kg CO<sub>2</sub>/GJ
- $\circ$  fuel @ \$0.04/kWh; η<sub>boiler</sub>=85%; EF=54 kg CO<sub>2</sub>/GJ
- $\circ$  carbon @ \$25/tonne CO<sub>2eq</sub>
- o 250 days operation per year



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#### Case Study - Meat Processing Without Rendering





Net Heat Flow (kW)

500

120

100

Case Study 1

Hot & Cold Utility	Discement	COP <sub>h</sub> or	Electricity	Fuel Use	Energy	CO <sub>2</sub> Emissions			
Options	Flacement	COPr	Use (kW)	(kW)	Cost (\$/h)	(kg/h; \$/h)			
Case Study 1 – Meat processing without rendering									
Boiler	370 kW <sub>t</sub> @ 100°C	-	0	435.3	\$17.41	84.6; \$2.12			
R717 Refrig.	240+190 kWr @ -30/-5/25°C (10.0 bar)	3.72	115.4		\$13.85	12.5; \$0.31			
Ambient	546 kW <sub>c</sub> @ 15°C		16.4	-	\$ 1.97	1.8; \$0.04			
			131.8		\$33.23	98.8; \$2.48			
R744 HP	71+190 kWr+370 kWh @ -30/-5°C/93.5 bar	5.80	108.8	8 <u>4</u> 0	\$13.06	11.8; \$0.29			
R744 Refrig.	169+0 kWr @ -30/-5/25°C (64.3 bar)	2.36	71.5*	*58.9kWe	\$ 8.58	7.7; \$0.19			
Ambient	240 kW <sub>c</sub> @ 15°C	. <del></del>	7.2	(if R717)	\$ 0.86	0.8; \$0.02			
2			187.5	· · · · ·	\$22.50	20.3; \$0.51			
R717 HP	250+120 kWh @ 25/51/89°C (50.1 bar)	6.92	53.5		\$ 6.42	5.8; \$0.14			
R717 Refrig.	240+190 kWr @ -30/-5/25°C (10.0 bar)	3.72	115.4	121	\$13.85	12.5; \$0.31			
Ambient	229 kWc @ 15°C	120	6.9		\$ 0.83	0.7; \$0.02			
			175.8		\$21.10	19.0; \$0.47			



- Trans-critical R744 (refrig+heating)
  - saves \$12.70/h over boiler +R717 refrig
  - \$109k higher capital (1.4 year payback)
- R717 Refrig + R717 or R134a HP
  - saves \$14.40/h over boiler + R717 refrig
  - \$307k higher capital (3.6 year payback)



#### Case Study - Meat Processing With Rendering

Hot & Cold Utility	Discement	COP <sub>h</sub> or	Electricity	Fuel Use	Energy	CO <sub>2</sub> Emissions
Options	Flacement	COPr	Use (kW)	(kW)	Cost (\$/h)	(kg/h; \$/h)
Boiler	692 kWt @ 135°C	Ť -	0	814.1	\$32.56	158.3; \$3.96
R717 Refrig.	240+190 kWr @ -30/-5/25°C (10.0 bar)	3.72	115.4	(=)	\$13.85	12.5; \$0.31
Ambient	$227 \text{ kW}_{c} + 545 \text{ kW}_{c}$ @ $15^{\circ}\text{C}$		23.2	1	\$ 2.78	2.5; \$0.06
			138.6		\$49.19	173.3; \$8.29
Boiler	440 kWt @ 135°C		-	517.6	\$20.70	100.6; \$2.52
R718 HP (open)	$227 \text{ kW}_{c} + 252 \text{ kW}_{h} @ 100/130^{\circ}\text{C} (3 \text{ stage})$	9.97	25.3	-	\$3.04	2.7; \$0.07
R717 Refrig.	240+190 kWr @ -30/-5/25°C (10.0 bar)	3.72	115.4	-	\$13.85	12.5; \$0.31
Ambient	546 kWc @ 15°C	-	16.4	120	\$1.97	1.8; \$0.09
			157.1		\$39.56	117.6; \$2.99
R718 HP (open)	623 kWc+692 kWh @ 100/130°C (3 stage)	9.97	69.5	170	\$8.34	7.5; \$0.19
R744 HP	87+190 kWr+397 kWh @ -30/-5/96.1 bar	3.66	184.2	-	\$22.10	19.9; \$0.50
R744 Refrig.	153+0 kWr @ -30/-5/25°C (64.3 bar)	2.36	64.7*	*53.3kWe	\$7.76	7.0; \$0.17
Ambient	218 kW <sub>c</sub> @ 15°C	-	6.5	(if R717)	\$0.78	0.7; \$0.02
device the solution of the sol			324.9		\$38.99	35.1; \$0.88
R718 HP	227 kW <sub>c</sub> + 261 kW <sub>h</sub> @ 95/135°C (4 stage)	7.60	34.3		\$4.12	3.7; \$0.09
R718 HP+	353 kWc + 431 kWh@ 80/135°C (5 stage)	5.55	77.6		\$9.31	8.4; \$0.21
+R717 HP	260 kW <sub>c</sub> + 353 kW <sub>h</sub> @ 25/51/85°C (46.1 bar)	3.77	93.6	-	\$11.23	10.1; \$0.25
R717 Refrig.	240+190 kWr @ -30/-5/25°C (10.0 bar)	3.72	115.4		\$13.85	12.5; \$0.31
Ambient	286 kW <sub>c</sub> @ 15°C	-	8.6		\$1.03	0.9: \$0.05
	ACTU SEL SERVICIPE SERVICE ALL DATA		329.5		\$39.54	35.6; \$1.78
Boiler	415 kWt @ 135°C		1.5	488.2	\$19.53	94.9; \$2.37
R1336mzz(Z) HP	227 kW <sub>c</sub> + 277 kW <sub>h</sub> @ 95/135°C (14.9 bar)	5.50	50.3	-	\$6.04	5.4; \$0.14
R717 Refrig.	240+190 kWr @ -30/-5/30°C	3.72	115.4	-	\$13.85	12.5; \$0.31
Ambient	546 kW <sub>c</sub> @ 15°C	-	16.4	-	\$1.97	1.8; \$0.09
	ini anit internationalitationent inter		182.1		\$41.39	114.6; \$2.87





- R718 HP+R717 refrig (or R718 HP+R744 HP/Refrig)
  - o saves \$14.90/h (\$17.61/h) over boiler+R717 refrig
  - o \$252k (\$812k) higher capital so 2.8 year (7.7 year) payback



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#### Case Study - General Food Processing

Hot & Cold Utility Options	Placement	COP <sub>h</sub> or COP <sub>r</sub>	Electricity Use (kW)	Fuel Use (kW)	Energy Cost (\$/h)	CO <sub>2</sub> Emissions (kg/h; \$/h)
Boiler+Cogen R717 Refrig. Ambient	1625+1500 kWt @ 87/150°C 1500 kWr @ 5/25°C 4725 + 1656 kWc @ 15°C	9.59	-203.0 156.4 <u>191.4</u> 144.8	3915	\$132.24 \$18.77 <u>\$22.97</u> \$173.98	739.2;\$18.48 16.9; \$0.42 <u>20.7; \$0.52</u> 776.7;\$19.42
Boiler Hybrid HP (x=0.5) R717 Refrig. Ambient	1500 kW <sub>r</sub> @ 150°C 1299 kW <sub>c</sub> @ 2.92 bar; 31-51°C+ +1625 kW <sub>h</sub> @ 11.7 bar; 70-95°C 1500 kW <sub>r</sub> @ 5/25°C 3426 kW <sub>c</sub> + 1656 kW <sub>c</sub> @ 15°C	4.98 9.59	0 326.2 156.4 <u>152.5</u> 635.1	1765 - - -	\$70.60 \$39.14 \$18.77 <u>\$18.30</u> \$146.81	343.1; \$8.58 35.2; \$0.88 16.9; \$0.42 <u>16.5; \$0.41</u> 411.7;\$10.29
Boiler R717 HP R717 HP R717 Refrig. Ambient	1500 kWt @ 150°C 700 kWc+906 kWh @ 40/92°C (53 bar) 567 kWc+719 kWh @ 32/80°C (41 bar) 1500 kWr @ 5/25°C 3458 kWc + 1656 kWc @ 15°C	4.39 4.72 9.59	0 206.2 152.2 156.4 <u>153.4</u> 668.2	1765 - - -	\$70.60 \$24.74 \$18.26 \$18.77 <u>\$18.41</u> \$150.78	343.1; \$8.58 22.3; \$0.56 16.4; \$0.41 16.9; \$0.42 <u>16.6; \$0.41</u> 415.3;\$10.38



- Hybrid R717+R718 HP best match for heating & cooling near pinch (COP=5)
  - saves \$36.30/h over boiler+cogen+R717 refrig
  - \$1,652k higher capital so 7.6 year payback
- HP heating at 150°C not economic as residual heat source <32°C (e.g. R717+R718 cascade has COP=2.4)



#### Case Study - Dairy Powder Processing

Hot & Cold Utility	Placement	COP <sub>h</sub> or	Electricity	Fuel Use	Energy	CO <sub>2</sub> Emissions
Options		COPr	Use (kW)	(kW)	Cost (\$/h)	(kg/h; \$/h)
Boiler+Cogen	4274+4050+4329 kWt @ 100/150/205°C		-1235	16339	\$505.36	3043;\$76.07
Ambient	8640 kW <sub>c</sub> @ 15°C	-	259.2	-	\$31.10	28.0; \$0.70
	vicional de la constante de la		-975.8		\$536.46	3071;\$76.77
Boiler	4217 kWt @ 205°C	-	0	4961	\$198.44	964.4;\$24.11
R718 HP	1550 kW <sub>c</sub> + 1634 kW <sub>h</sub> @ 66/79.3°C (2 stage)	19.6	83.6	-	\$10.03	9.0; \$0.23
Hybrid HP	4447 kW <sub>c</sub> @ 7.5 bar; 17.8-34.6°C	2.89	2359	-	\$283.08	254.8; \$6.37
(x=0.95)	6805 kW <sub>h</sub> @ 63 bar; 79-174°C			<b>1</b> 50	-	-
Ambient	2643 kW <sub>c</sub> @ 15°C	-	79.3	-	\$9.52	<u>8.6;</u> \$0.21
			2521.9		\$501.07	1237; \$30.92
Boiler	4217 kWt @ 205°C	-	0	<mark>4961</mark>	\$198.44	964.4;\$24.11
R718 HP	1550 kW <sub>c</sub> + 1634 kW <sub>h</sub> @ 66/79.3°C (2 stage)	19.6	83.6	-	\$10.03	9.0; \$0.23
R718 HP+	$5797 \text{ kW}_{c} + 6805 \text{ kW}_{h} @ 80/160^{\circ}\text{C} (7 \text{ stage})$	6.75	1008	-	\$120.96	108.9; \$2.72
+R717 HP	2140+2140 kW <sub>c</sub> +5797 kW <sub>h</sub> @ 18/24/85°C	3.82	1518	<b>1</b>	\$182.16	163.9: \$4.10
Ambient	2810 kW <sub>c</sub> @ 15°C	-	84.3	-	\$10.12	<u>9.1; \$0.23</u>
	100 0 <b>7</b> 0.0		2693.9		\$521.71	1255; \$31.38



- R718 HP near pinch is cost-effective (COP=19.6)
- For heating up to 150°C
  - Hybrid R717+R718 HP has COP=2.9 but high pressure
  - R717+R718 cascade (9 stages) has COP=2.7 but complex
  - $\circ$  > \$150/tonne CO<sub>2eq</sub> required to get payback < 5 years







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### HP Feasibility - Spray Drying



# Conclusions

- High potential for existing HP technology <~130°C
- Electrical upgrade can be an extra constraint
- HPs marginal for residual heating common in NZ after heat recovery because

 $\circ$  sinks > 120°C

- $\circ$  sources at or just above ambient
- Matching temperature profiles help get higher COPs
- Thermodynamic limits mean usually COP<3
- Need > 150/tonne CO<sub>2eq</sub> for HTHP to be feasible
- NZ lacks experience with HTHPs
- Other low carbon process heating sources are also highly constrained







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# Questions



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